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ANALYSIS OF DYNAMIC CHARACTERISTICS OF SHORT JOURNAL BEARINGS - A REVIEW

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ABSTRACT

The stability of bearing-rotor system is a very important problem for design, manufacturing, and operation of rotating machinery. The instability of rotor system will result in the strong vibration and even disastrous accident of machinery. The researches for decades indicate that the strong-nonlinear exciting sources such as oil-film forces, sealing forces and non uniform steam forces etc. all are main reasons which can make unstable accidents in rotating machineries. The oil-film forces are the leading nonlinear exciting source which makes the bearing rotor system to be a self-exciting vibration system and results in fatal accidents. So solution of nonlinear oil-film forces in sliding bearings is always very important for dynamic analysis of rotor-bearing system. The computational methods of bearing nonlinear fluid-film forces must be studied to carry out the nonlinear dynamic analysis of rotor systems and widely reveal the operation laws of large-scale rotating machineries. It has very important theoretical significance for advancing the stability, safety and reliability of rotating machineries.

KEYWORDS: bearing, reliability, rotating machineries, Stability, vibration.

Introduction

As of late, as fast revolving machines with roller heading discovered wide applications, their flow properties were broadly contemplated. As a continually expanding interest is postured to their running exactness and pace, substantially more consideration is paid to the vibration investigation of the rotors upheld by roller direction. In addition, as a wellspring of vibration, the roller direction pull in solid scholarly concerns due to their nonlinearity because of the Hertzian power twisting relationship, the spiral clearances and the bearing waviness.[1] Increasing requests for elite turning hardware have made the rotor dynamic issues more intricate, and more consideration has been drawn on rotordynamics. Displaying and PC reproduction innovation have been generally utilized as a part of outlining and breaking down rotorbearing frameworks. A multi-bearing rotor framework is statically uncertain. Its dynamic conduct relies on upon the relative positions of the direction and the properties of its subsystems. [4]The relative positions of heading are generally alluded to as framework design or bearing arrangement. Along these lines, the dynamic properties of a multi-bearing rotor framework are a component of the turning pace and the framework configuration. [4] The motion of a rotor framework upheld by liquid film heading is naturally a nonlinear issue. Both linearized strategies and non-straight methodologies have been utilized as a part of the displaying and taking care of rotor element issues. Linearized models are regularly utilized as a part of expectations of basic velocities, vibration reaction and unsteadiness limit in a vast scope of working focuses. Non-direct models are utilized not just to confirm results acquired from linearized model, additionally to study some essential rotor-bearing element phenomena. These phenomena, for example, sub-consonant reverberation and point of confinement cycles can't be seen without representing exceedingly non-direct powers delivered by liquid film course under huge abundance vibrations.[4]

keeping in mind the end goal to grow superior turning apparatus, dynamic vibration control has been paid developing considerations to enhance the framework dynamic properties by utilizing dynamic devices.[4]

DESCRIPTION OF THE ACTIVE JOURNAL BEARING

The adaptable sleeve can be considered as another element of the proposed dynamic diary bearing as indicated in Fig. 1. The sleeve is initiated by the chamber weight pc which is controlled by valves in the water powered framework. The oil film of the bearing is isolated from the weight chamber by the adaptable seal. Thusly, the chamber weight won't impact the limit states of the oil film. The deformity of the adaptable sleeve can be changed by changing the chamber weight. Subsequently the geometry and thickness of the oil film, and henceforth the dynamic properties of the rotor framework, can be controlled without ceasing the operation of the machine. The chamber weight can likewise be changed powerfully by a servo valve. So the dynamic diary bearing can convey element control powers to the rotor through the oil film to control the constrained vibration by either an open-circle means or input approaches. [4]

NUMERICAL MODEL OF SYSTEM

Fig.1 demonstrates the schematic chart of the double rotor framework. The left hand of higher weight rotor an is bolstered by two same rakish contact Bearings 1, 2 and the right hand of lower weight rotor b is upheld by two distinctive profound section metal rings 3, 4, where Bearing 4 is the intershaft bearing. The double rotors have distinctive co-turning paces. [2]

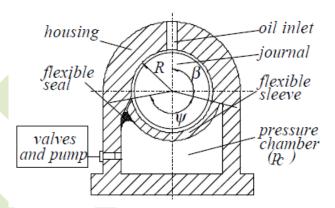


Fig 1.Schematic of the active journal bearing

The coupling between the two rotors through the inter shaft bearing is likewise considered in the scientific model. The scientific model takes after two stages. Above all else, the removals, flexible diversions and contact powers of the direction are ascertained considering 5-DOF of the rotors. At that point the movement mathematical statements of the double rotors are defined in view of rotor dynamics. [2]

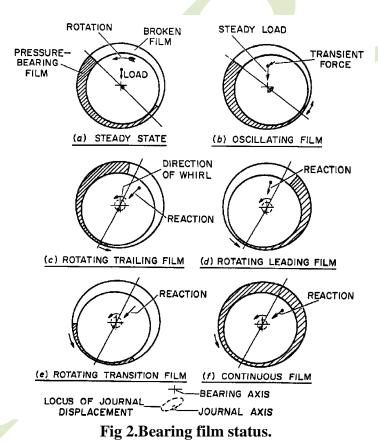
DISAPPOINTMENT OF SYSTEM

All pivoting hardware is bolstered by one or more heading, which have basic influence of the whole framework, since it is the segment that allows the relative movement between the stationary and moving parts. There are two general sorts of direction which are usually utilized as a part of rotor-bearing framework applications. [3] These are liquid film heading and moving component course. Heading can have a huge impact on machine's vibration attributes. The liquid film of a fluid film bearing acts like a

spring-damper framework and it impacts the machine discriminating rates and irregularity reaction. Also, bearing liquid film strengths can bring about rotor shakiness that outcome in genuine levels of self-energized vibration. Shaft seals have a comparable impact as liquid film bearings[3]. They impact the basic paces, can give damping or then again cause unsteadiness. Insecurity from liquid film direction and shaft seals emerges from the way that amid spiral relocation of the rotor a restoring power is created, which has a part at right points to this displacement.[3] by and by, shakiness must be evaded and one must know however much as could be expected about the conditions and about conduct amid flimsiness. In this way, in the accompanying areas the solidness of rotor-bearing frameworks is considered. Beginning with the most basic rotor demonstrate that is bolstered in two unbending course at its finishes, more reasonable and more included cases are considered by fusing the impacts of adaptable bearings. [3]

Synchronous spin is the characteristic recurrence of the framework at which self-left vibration happens. Frequently in building it is obliged to get a speedy estimate of the arrangement. Strategies for getting basic answer for acquire the normal recurrence:

- i. Dunkerley's equation,
- ii. Energy technique (Rayleigh's principle)[5]



STABILITY CONSIDERATIONS OF ROTOR-BEARING SYSTEMS

The material in this area is given to present and clarify the way of rotordynamic phenomena from nearly straightforward expository models. The phenomena showed by adaptable rotors and methods utilized for their examination is fundamentally like different ranges of vibrations and basic dynamics.[3] The vibration issues can be spoken to by the comparison of movement .

$$MX&& + CX& + KX = F(t)$$
 (1)

The basic symphonious vibration of the rotor is portrayed with the terms MX&& and KX of the above mathematical statement. Damping, either from the structure of the pole or from the bearing structure is portrayed by the term CX&. Imbalanced rotor impacts are portrayed by the driving term F(t) on the right hand side. Adaptable course, hydrodynamic direction and gas seals present terms of the structure KX and CX&. The complete arrangement of Eqn. (1) comprises of the arrangement of the homogeneous mathematical statement together with the specific arrangement comparing to the right-hand side. Arrangement of the homogeneous comparison requires the eigenvalues of the framework to be found. These are conjugate mind boggling or genuine and describe the common vibration.[3] The nonexistent part compares to the characteristic recurrence being referred to and the genuine part gives the steadiness of the regular vibration. For a negative genuine part, the vibration rots with time that implies the framework is stable, what's more, for positive genuine part it develops which implies it is insecure. The solidness limit of the framework is come to when the genuine piece of an eigenvalue is zero.

MODELING AND ANALYSIS OF MOTION OF A LABORATORY TEST RIG

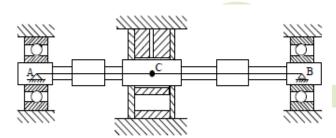


Fig 3.A three-bearing rotor test rig.

The techniques developed above have been employed to a laboratory test rig as shown in Fig. 3. The rig is a three-bearing rotor system. The rotor is two meters long and weighs 11.24kg. The active bearing is located 663mm from the left ball bearing and 1037mm from the right one. Some other parameters of the test rig are: bearing diameter D=50mm; bearing length to diameter ratio L/D=0.8; bearing nominal radial clearance c=0.3mm; $b=105^{\circ}$ and $Y=160^{\circ}$ (see Fig. 1 and Fig. 2); thickness of the flexible sleeve d=5mm; lubricant viscosity h=0.04 Pascal×Sec.[4] The rotor was modelled by the FEM with 26 elements and 104 DOF. The final condensed model contains only three rotor stations with only 6 DOF. The flexible sleeve was divided evenly into 20 elements with 60 DOF. The final condensed model contains only three sleeve stations with 3 DOF. It has been found that the final condensed models have almost identical eigenvalues and eigenvectors to the original FEM models up to the second mode for both the rotor and the flexible sleeve. [4]

STRENGTH ANALYSIS

In some particular applications, plain round about bearing is basically supplanted by some different heading, as plain bearing does not suit the steadiness prerequisites of fast machines and exactness machine tools.[5] Grooved round direction and multi-flap course with two flaps, three projections and four flaps are usually utilized. The content takes after gives knowledge into nonlinear transient investigation of multi flap diary bearing frameworks. The minimum amount parameter (a measure of steadiness) is assessed for different estimations of perspective proportions other than figuring out the consistent state attributes of multilobe diary heading (two furrowed, two flap, three projection and four projection, for example, burden bearing limit, Sommerfeld number and disposition angle[5]

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EXAMINATION OF INSTABILITY

The vibration sign, portraying the rotor movement, is a perplexing sign. The genuine piece of this sort of signs is rotor relocation in the X-course while the fanciful part is a removal in the opposite heading, as we say in the Y-bearing. An instrument for examination is a full range, which comes about because of the Fourier change of the mind boggling sign. The full multispectra of the rotor keep running up and drift down are utilized to assess a size as an element of the rotor revolution speed. The multispectrum cuts serve to check of the improved scientific model of a rotor framework and to examine the rotor vibration utilizing a system in light of the Nyquist steadiness basis. As it is no doubt understood the self-energized vibration, called liquid instigated vibration, happens when the rotor turn pace crosses a certain threshold. The new term is a full range. The full range is a decent instrument for soundness examination of rotors bolstered by liquid film direction. Favourable position of the full range is that this two-side range portrays movement in the plane while the one-side range depicts movement along a straight line. The two-side range permits assessing the circle envelope. The main piece of the paper shows spin vibration and the autonomy of the proportion relating the precession pace to the rotor rotational speed on the rotor total rotational velocity. The lumped parameter model of the diary focus movement in the diary bearing gives clarification of the soundness edge and the onset of the self-energized vibration. The examination of the diary conduct is taking into account utilizing the Nyquist steadiness model for direct element systems. [6]

CONCLUSION

The introduced numerical model can be utilized to foresee dynamic practices of multi-bearing rotor frameworks consolidating the exhibited dynamic diary bearing. Arrangements got from the non-straight and linearized models are steady. The linearized model is uniquely suitable for a general examination of the framework qualities more than an extensive variety of framework arrangement parameters and the turning speed in which various mixes of design parameters should be dissected. Eigenvalue investigation in light of the linearized model gives data of basic spees and flimsiness edges in the meantime, while one example arrangement of the non-straight comparisons of movement by numerical combination obliges a significant registering time. Numerical recreations taking into account the non-straight model give not just a measure to confirm the legitimacy of results from the linearized model, it additionally gives some critical data about the framework, e.g. the points of interest of the subharmonic spinning movement of the diary brought on by the bearing oil film and breaking point cycles which can't be acquired from the linearized model.[4] Computation time can be enormously lessened by utilizing the Guyana buildup strategy. It really made the arrangement by numerical mix of the non-straight comparisons of movement doable in the computations introduced in this paper. The grew non-straight and linearized comparisons of movement were likewise utilized as a part of control law blend in constrained vibration control by the proposed dynamic diary bearing utilizing both an open-circle methodology and a criticism system.[4]

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REFERENCES

- [1] Wang Liqin, Cui Li, ZhengDezhi, GuLe, Nonlinear, Dynamics Behaviors Of A Rotor Roller Bearing System With Radial Clearances And Waviness Considered, Chinese Journal Of Aeronautics 21(2008) 86-96J.
- [2] Hu Qinghua, Deng Sier, TengHongfei, A 5-Dof Model For Aeroengine Spindle Dual-Rotor System Analysis, Chinese Journal Of Aeronautics 24 (2011) 224-234.S.
- [3] Z. A. Parszewski& J. M. Krodkiewski, *Machine Dynamics In Term Of The System Configuration Parameters*, Proceedings Of The International Conference On Rotor Dynamics, 1986, Tokyo, Japan, Pp. 239-244.

- [4] J. W. Lund, *Stability And Damped Critical Speeds Of A Flexible Rotor In Fluid Film Bearings*, Trans. Asme, Journal Of Engineering For Industry, 1974, Vol. 96, Pp. 509- 517.
- [5] M. L. Adams, *Non-Linear Dynamics of Flexible Multi-Bearing Rotors*, Journal Of Sound And Vibration, 1980, Vol. 71, No. 1, Pp. 129-144.
- [6] G. Schweitzer, *Magnetic Bearings, Rotor dynamics 2: Problems In Turbo machinery*, 1988, Springer Verlag Wien-New York, Pp. 543-570.
- [7] A. B. Palazzolo, R. R. Lin, R. M. Alexander, A. F. Kascak, & J. Montague, *Test And Theory For Piezoelectric Actuator*³/₄Active Vibration Control Of Rotating Machinery, Trans. Asme, Journal Of Vibration And Acoustics, 1991, Vol. 113, Pp. 167-175.

