# THE EFFECTIVE ATOMIC NUMBERS AND THE EFFECTIVE ELECTRON NUMBERS OF SOME STEELS AT DIFFERENT GAMMA ENERGIES

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### ABSTRACT

In this study, the effective atomic numbers ( $Z_{eff}$ ), the effective electron number ( $N_{eff}$ ), the half value layer (HVL) and the mean free path ( $\lambda$ ) for two different steels have been determined at Co-60 and Eu-152 energies. The measurement of linear attenuation coefficients at 122, 245, 344, 444, 779, 867, 964, 1112, 1173, 1333 and 1408 keV energies was made using a gamma spectrometer system with a NaI (Tl) detector connected to Multi-Channel-Analyzer (MCA). The experimental half value thickness and the mean free path were found to be in good agreement with the calculation results. Also, effective atomic numbers ( $Z_{eff}$ ) and effective electron number ( $N_{eff}$ ) parameters were calculated using the EpiXS 2021 and the results were evaluated.

Keywords- The cross sections, effective atomic numbers, stainless steels, half value layer, mean free path.

# **1. INTRODUCTION**

With increasing energy demand and advancement in technology, the use of radiations is increasing rapidly in our daily lives. The use and applications of  $\gamma$  rays are increasing rapidly in various fields such as nuclear and radiation physics, industry, medicine, power generation and agriculture [1]. In addition to the many great advantages and benefits that nuclear technology provides to humanity, there are also some disadvantages assciated with radiation.  $\gamma$  radiation and high energetic x-rays are used in radiotherapy for cancer treatment in order to destroy unhealthy tissues along with the cancer cells in human body [2,3]. The photon mass attenuation coefficient, Z<sub>eff</sub>, and the N<sub>eff</sub> are the fundamental quantities in determining the penetration of X and  $\gamma$ -ray in matter [4, 5, 6, 7].

These highly penetrating and high energy ionizing radiations are harmful to the human body, sensitive laboratory equipment, animals, and environment. Therefore, it is important to study  $\gamma$  radiation in applied radiation fields, medical physics involving radiation for therapeutic and diagnostic use, radiation physics, reactors shielding etc. [2, 3, 8,9]. The study of highly penetrating gamma photons and interactions of highly energetic photons with different type of materials is also of prime importance in basic physics.

The carbon steel and stainless alloys are the common structural materials of nuclear reactors for calandria shell, end shield for primary heat transport system and moderator system [10,11]. Due to the development of nuclear technology over time, various beneficial applications of different types of radiations in medicine, industry, agriculture, and research as well as for nuclear energy production are increasing day by day. However, a disadvantage of these peaceful uses of radiation is that a harmful effect can be observed if the radiation is exposed to the personnel including other people nearby, beyond the allowable dose limit. When radiation is exposed to tissues or organs, it loses some its energy through different kinds of interactions and

this loss of energy may ionize the atoms of the cell, destroying the normal chemical equilibrium of the cell and eventually can bring death to the cell [12]. Therefore, the radiation must be attenuated enough to protect the personnel from the harmful effects caused by it also enable them to work by using an opposite shielding material. In the case of special purpose of radiation shielding lead and steel can be used as heavy weight aggregates.

The aim of this our study is to provide available information concerning using this kind of steel as a gamma shielding in nuclear applications. The well-known WinXCom program is usually employed for calculating gamma-ray and X-ray attenuation coefficient and interaction cross sections of different materials [13]. The most widely used platform for photon cross sections or mass attenuation coefficients is the XCOM [14] web program developed by NIST. Some researchers have also constructed PC-based software counterparts to XCOM, using the XCOM/NIST libraries [15, 16]. Any available computer code built on other major photon libraries that are distinct from XCOM/NIST has been scarce. An instance of such is a recent spread sheet program described in Hila et al. [17] that uses the EPICS2017 and the EPDL97 libraries to calculate mass attenuation coefficients, Z<sub>eff</sub> and N<sub>eff</sub>.

In this study, WinXCom program is used to calculate the partial and total mass attenuation coefficients for different compositions of Maraging steels at photon energies (1 keV-1 GeV). The mass attenuation coefficient data were then used to obtain the half value layer (HVL) and mean free path ( $\lambda$ ) of the investigated materials and were compared with the measurements obtained at photon energies of 122, 245, 344, 444, 779, 867, 964, 1112, 1173, 1333 and 1408 keV for two different steels, namely stainless steel (S1: EN 10204) and speed steel (S2: 2367). Also the Z<sub>eff</sub> and the *N*<sub>eff</sub> of the investigated materials were obtained by using EpiXs program [18].

## 2 MATERIALS AND METHODS

The  $\mu/\rho$  of two different types of steel, calculated using the XCOM code which uses chemical parameters of a mixture materials providing total cross sections as well as partial cross sections for various interaction processes at photon energy of 1 keV-100 GeV [15].

The detection of  $\gamma$ -rays was carried out using a gamma spectrometer consisting of a 10 cm diameter NaI(Tl) detector connected to the Multi-Channel-Analyzer (MCA). With the known density ( $\rho$ ) of a material, the mass attenuation coefficients ( $\mu/\rho$ ) were obtained via measuring the linear attenuation coefficients. The theoretical  $\mu/\rho$  values for the present steels were obtained by winXCcom program [19].

#### 2.1. Linear and mass attenuation coefficient

When a gamma-ray beam passes through an absorber, the intensity of the beam will be reduced according to the Beere-Lambert's law:

$$I = I_0 \exp(-\mu x) = I_0 \exp(-\frac{\mu}{\rho}\rho x)$$
(2.1)

where *I* and  $I_0$  are the attenuated and incident gamma ray intensities, respectively. *x* is the thickness of the sample in cm,  $\mu$  (cm<sup>-1</sup>) is the linear attenuation,  $\rho x$  is are the material thickness in g/cm<sup>2</sup> and  $\rho$  is the material density and  $\mu/\rho$  is the mass attenuation coefficient in cm<sup>2</sup>/g [20, 21].

The half value layer *HVL* is the thickness of the material where one half of the incident photons is attenuated. It can be calculated via [21, 18]

$$HVL = \frac{0.693}{\mu} \tag{2.2}$$

Last parameter to be calculated is tenth value layer TVL is the thickness of the shielding material where one tenth of the incident photons is attenuated

$$TVL = \frac{2.3026}{\mu} \tag{2.3}$$

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Linear attenuation coefficient is  $\mu = \rho \mu_m$  and mean free path is

$$\lambda = 1/\mu$$
 (2.4)

### 2.2 Effective atomic number and effective electron density

The mass attenuation coefficient for the compound or mixture can be derived from the coefficients of the compenent elements that are assumed to contribute to the weighted average [23, 24] (Hubbell and Seltzer, 1982, 1995):

$$\left(\frac{\mu}{\rho}\right) = \sum_{i} w_i (\mu/\rho)_i \tag{2.5}$$

where  $w_i$  and  $(\mu/\rho)_i$  are the fractional weight and the mass attenuation coefficient of the *i* th constituent element, respectively.  $(\mu/\rho)$  does not depend on the phase (gas, liquid, or solid) of the material. Therefore, it is useful to define the  $\mu/\rho$ . This mixing rule is valid assuming that the effects of molecular binding and the chemical crystalline environment are negligible. The  $\mu_m = (\mu/\rho)$  value of the alloys can be calculated for a given energy range using WinXCom software based on the mixture [19].

For a chemical compound or mixture, the fraction by weight  $(w_i)$  is given by,

$$w_i = \frac{A_i n_i}{\sum_j A_j n_j} \tag{2.6}$$

where A<sub>i</sub> is the atomic weight of the ith element and n<sub>i</sub> is the number of formula units and  $\sum_i w_i = 1$ .

Total photon interaction cross-section ( $\sigma_t$ ) of the compound is determined with the help of the mass attenuation coefficient ( $\mu_m$ ) through the following equation:

$$\sigma_t = \frac{\sum A_i n_i}{N_A} \mu_m \tag{2.7}$$

 $A_i$  is the atomic weight of the *i*th element,  $n_i$  the number of formula units of a molecule and  $N_A$  is Avogadro's number.

The molecular cross section can be computed utilizing the above  $\mu/\rho$  quantity as below

$$\sigma_{t,m} = \frac{1}{N_A} \left(\frac{\mu}{\rho}\right)_{comp} \Sigma(n_i A_i)$$
(2.8)

where  $N_A$  is the Avogadro number,  $n_i$  and  $A_i$  represent the number of element and atomic weight of the i th the element in the material, respectively. The total atomic cross-section ( $\sigma_{t,a}$ ) can be determined as follow: [25, 26, 27, 28].

$$\sigma_{t,a} = \frac{\sigma_{t,m}}{\sum n_i} \tag{2.9}$$

The total electronic cross-section ( $\sigma_{t,e}$ ) can be expressed as follow [22]

$$\sigma_e = \frac{1}{N_A} \sum \frac{f_i A_i}{Z_i} \left(\frac{\mu}{\rho}\right)_i \tag{2.10}$$

where  $f_i$  denotes the fractional abundance of the element *i* and  $Z_i$  the atomic number of constituent element and  $(\mu/\rho)_i$  is the total mass absorbtion coefficient of the element. The  $Z_{eff}$  is related to  $\sigma_a$  and  $\sigma_e$  through the following equation [4, 25, 29, 30]

$$Z_{eff} = \frac{\sigma_{t,a}}{\sigma_{t,e}} \tag{2.11}$$

The interpolation method is considered more complex to execute than the direct method because of required elemental database and the possibilities for multivalued  $Z_{eff}$  [18, 31, 32].

The effective electron density, (number of electrons per unit mass,  $N_{eff}$  of the sample can be calculated from the relation

$$N_{eff} = \frac{Z_e N_A}{A_{comp}} \sum n_i (electron/g)$$
(2.12)

$$N_{eff} = Z_{\text{eff}} \frac{N_A}{\sum f_i A_i} \tag{2.13}$$

Here A<sub>comp</sub> is the total atomic weight of the elements in the compound [18, 33].

The detector system including 10 cm diameter NaI(TI) detector by ORTEC Inc., connected to a multichannel pulse height analyzer are used. The sample was placed between the <sup>152</sup>Eu source and the detector. The measurements have been carried out in the range from 244 to 1528 keV. The measured photon attenuation coefficients  $\mu$ , *HVL*, *TVL* were compared with the calculations obtained by using XCom [19].

The mass attenuation coefficient,  $\mu_m$  (cm<sup>2</sup>/g) for four different types of steel, calculated using the WinXCom code which uses chemical parameters of a mixture materials providing total cross sections as well as partial cross sections for various interaction processes at photon energy of 1 keV-1 GeV. The computation of the mass attenuation coefficients of the above five sample materials has been carried out by the mixture rule by using the WinXcom software for the mentioned energy range to present a comparison between the calculated and X-com values.

In this study, a Windows-based application software named EpiXS 2021 (available at https://www.pnri.dost.gov.ph/index.php/downloads/software/epixs) was used to calculate Z<sub>eff</sub> and effective electron number. The software performs data library interpolation from 1 keV to 100 GeV and calculates partial or total cross sections ( $\sigma$ ), mass attenuation coefficients ( $\mu/\rho$ ), linear attenuation coefficients ( $\mu$ ), mean free paths (mfp), HVL, Z<sub>eff</sub>, and N<sub>eff</sub> calculates [18].

# 3. RESULTS AND DISCUSSION

For two different steels, the  $\mu/\rho$  have been calculated at photon energies of 1 keV-1 GeV and and experimental measurement results were compared for the photon energies from 122 keV to 1408 keV. agreement for the present steels. It was observed that the experimental results and the theoretical calculation results were in good agreement.



Fig 1. Experimental and calculated HVL for S1: EN 10204 and comparison with the experimental values (filled circle data).



Fig 2. Experimental and calculated HVL for S2: EN 2367 and comparison with the experimental values (filled circle data).

The  $Z_{eff}$  for concretes at photon energies of 1 keV–100 GeV have been calculated using EpiXS 2021 code and the results were displayed in Figure 3 and 4 as a function of photon energy. This could be the result of different interaction processes of photon with the material for different energy ranges. The dominating photon interaction process is photoelectric absorption at low energies, Compton scattering (mainly incoherent) at intermediate energies, and pair production gradually becomes the dominant interaction process above about 1 MeV. Almost a constant structure has been observed after this energy.



Figure 3 The Z<sub>eff</sub> of concretes as a function of photon energy, for S1 samples respectively.



Figure 4 The Z<sub>eff</sub> of concretes as a function of photon energy, for S2 samples respectively.

The effective electron numbers ( $N_{eff}$ ) for concretes at photon energies of 1 keV-1 GeV have been calculated using EpiXS 2021 code and the results were displayed in Figure 5 and 6 as a function of photon energy. The results found directly and by interpolation are also shown in these figures. The values of N<sub>eff</sub> found directly and by interpolation are between 100 keV and 7 MeV, while giving the same values, it differs below 100 keV and above 7 MeV.



Figure 5. The N<sub>eff</sub> of concretes as a function of incoming photon energy, for S1 and S2 samples respectively.



Figure 6. The  $N_{\text{eff}}$  of concretes as a function of incoming photon energy, for S1 and S2 samples respectively.

The  $Z_{eff}$  varies around 25 for S1 likewise, the  $N_{eff}$  varies around 3 for S1. However, for the S2 sample, both the  $Z_{eff}$  and the  $N_{eff}$  are almost constant.



Figure 7. The mean free path of concretes as a function of incoming photon energy,

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The photon means free paths ( $\lambda$ ) for concretes at the photon energies of 122, 245, 344, 444, 779, 867, 964, 1112, 1408, 1173 and 1333 keV have been calculated by using linear attenuation coefficients obtained from the measurements and the results were displayed in Figure 7 as a function of photon energy. It can be seen from this figure that the  $\lambda$  increased with the photon energy. As can be seen from Figure 9, the  $\lambda$  values calculated using WinXCom for samples S1 and S2 shows good agreement with the experimentally found values. It is very close to each other for the S1 and S2 samples in the energy region of interest. But, at energies above 3 MeV, the results obtained for S1 and S2 differ from each other.

# 4. CONCLUSION

According to the results obtained in this study, effective atom and electron numbers depend on the incident photon energies and the ratios of the materials in the compound. half vale layer (HVL) and the  $\lambda$  of concretes containing stainless steel (S1: EN 10204) and speed steel (S2: 2367). Z<sub>eff</sub> and N<sub>eff</sub> have been also calculated theoretically. In the interaction of photon with matter, the values of these parameters are dependent on the physical and chemical environments of the sample. The obtained mass attenuation coefficient values decrease with increasing photon energy. It was found that the experimental results of this work are in good agreement with the computed values. It could be concluded that the experimental results were consistent with the theoretical data. The results of this study will be helpful to understand better how mass attenuation coefficient values change with the variation in effective atomic numbers and effective electron densities of concretes.

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